

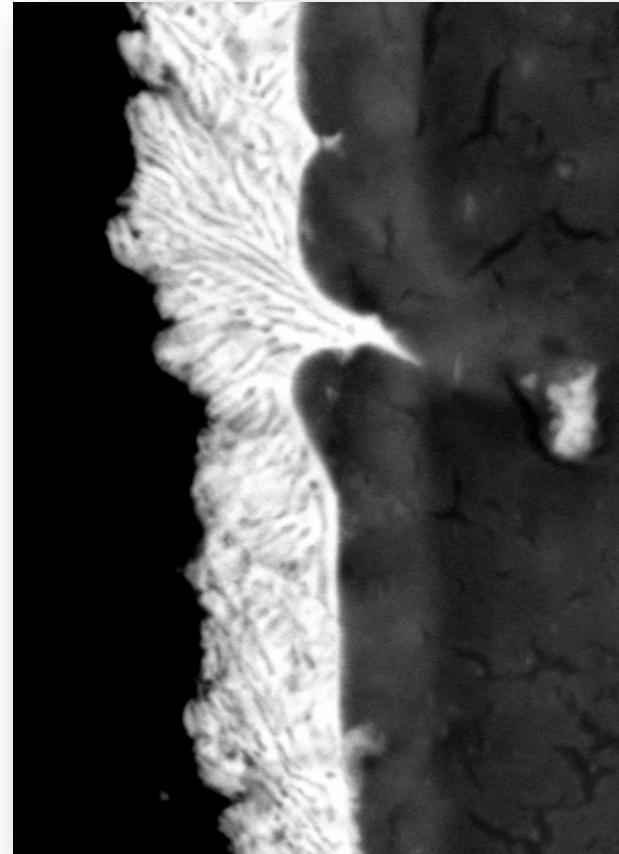
Diffusion in Solids and the Kirkendall-Effect

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Hypereutectic thermal treatment

- Heterogeneous
- Difficult to control
- Patterns forming during solidification



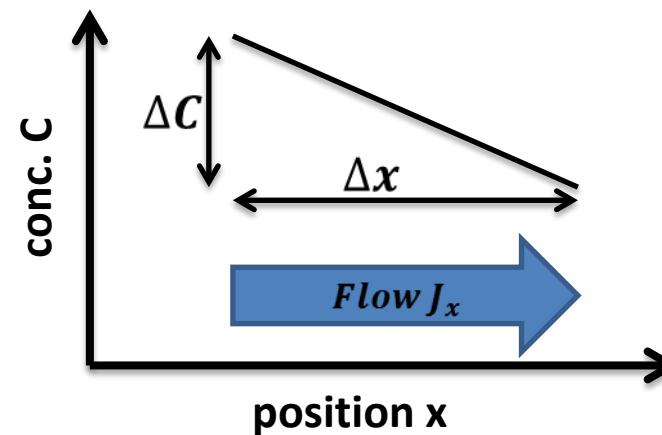
Fick's First Law

$$J_x = -D \frac{\partial C}{\partial x}$$

J_x = diffusion flux

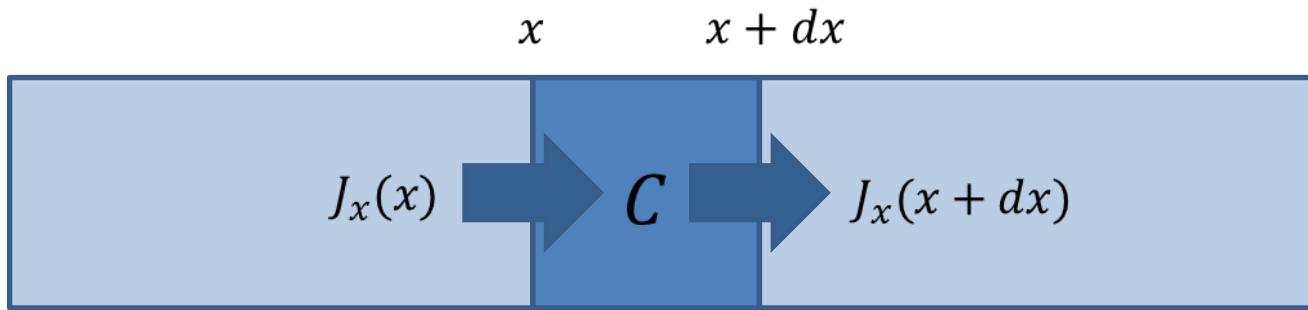
D = diffusion coefficient

C = concentration



Equation of Continuity

- Time dependency?



$$-\frac{\partial J_x}{\partial x} = \frac{\partial C}{\partial t}$$

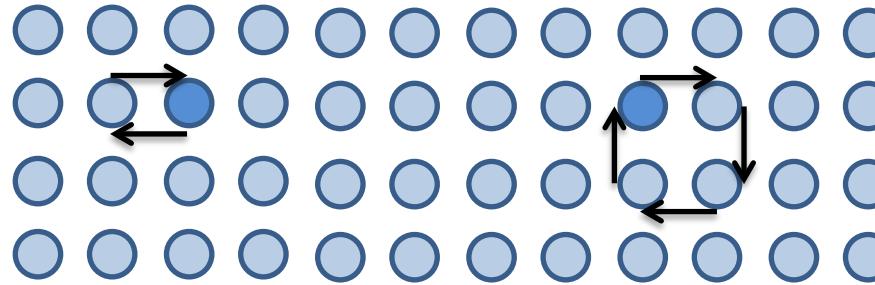
Fick's Second Law

$$\frac{\partial C}{\partial t} = \frac{\partial}{\partial x} \left(D \frac{\partial C}{\partial x} \right)$$

If D is independant of x :

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2}$$

Atomic Jump Process



Direct exchange?

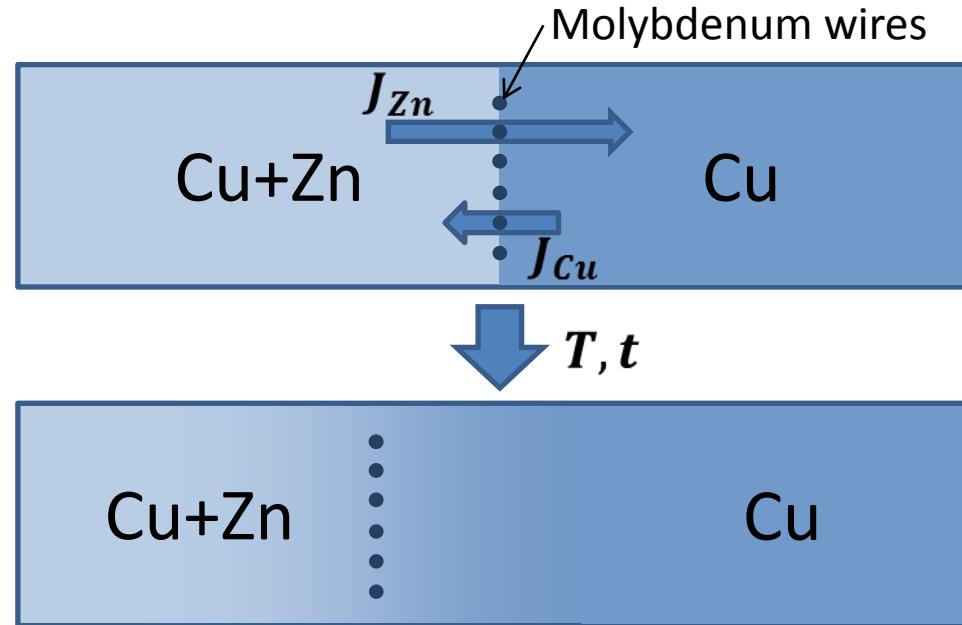
Ring exchange?

- Direct exchange requires a large distortion of the lattice and therefore has a high activation enthalpy
- Ring exchange requires less activation enthalpy but an unlikely collective motion



Those processes barely contribute to diffusion

Kirkendall Effect

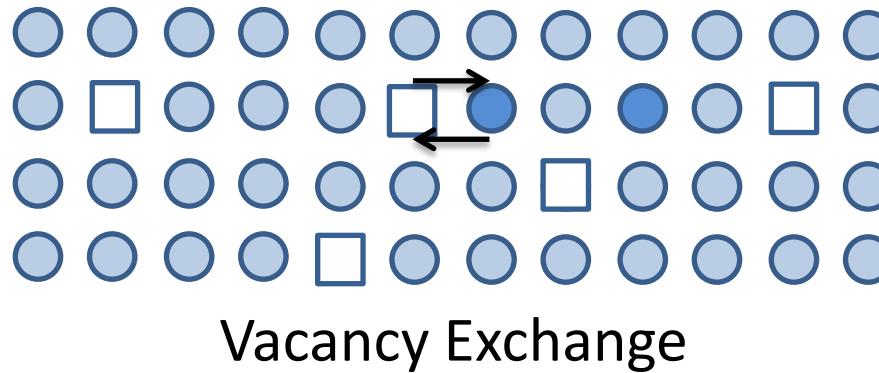


$J_{Zn} \neq J_{Cu}$ but direct or ring exchange would imply $J_{Zn} = J_{Cu}$

→ Another process must be responsible

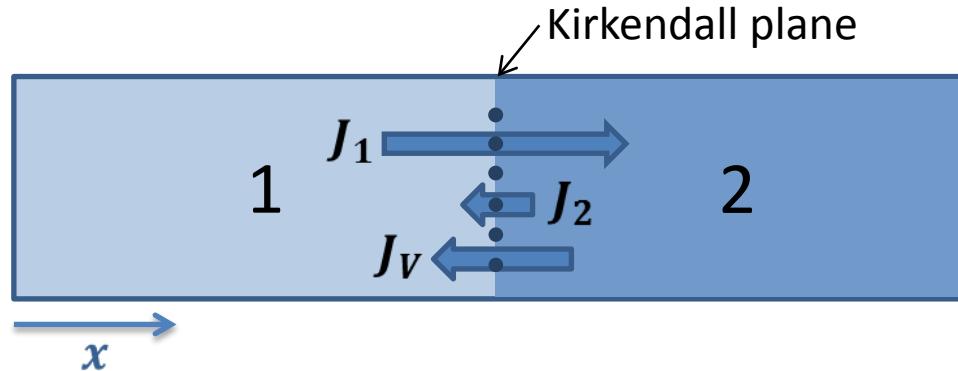
The Vacancy Mechanism

- Site fraction of vacancies lie around 10^{-3} and 10^{-4} near T_s



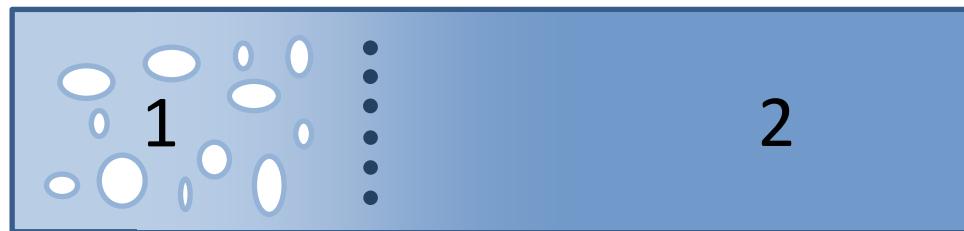
- Under normal conditions vacancy exchange is the main mechanism of diffusion

Kirkendall Voids



$J_1 > J_2 \rightarrow$ Net flow of metal atoms in x-direction

\rightarrow Vacancy flow J_V in negative x-direction



Kirkendall Voids (example)

$$J_{Cu} > J_{Ni}$$

Vacancy flow into original copper domain



(Choi, Matlock and Olson)

14 min
1000°C



(Choi, Matlock and Olson)

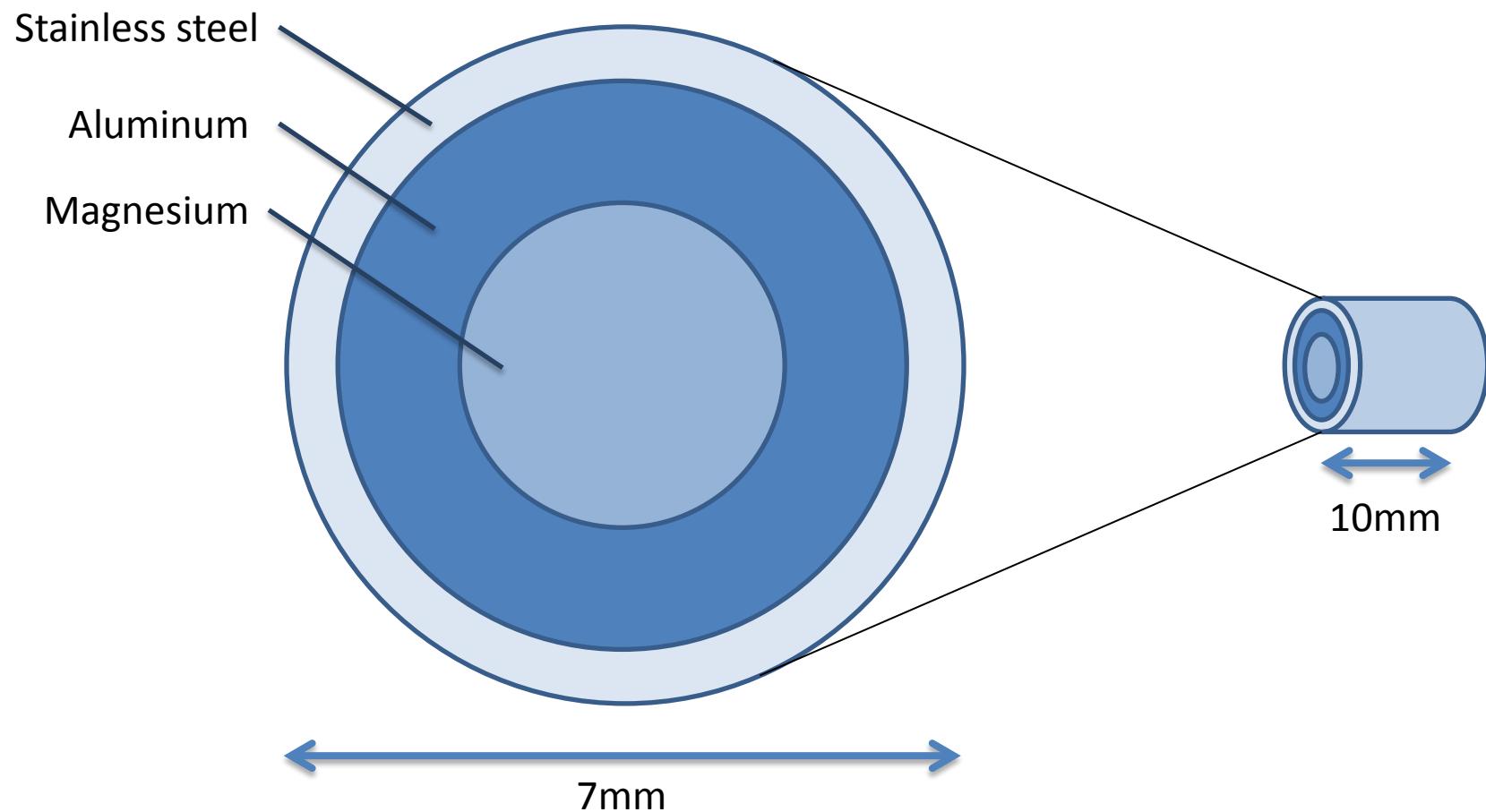
Aluminum-Magnesium binary alloy

- Better understanding of Al-Mg interdiffusion
- Measurement of the interdiffusion coefficient

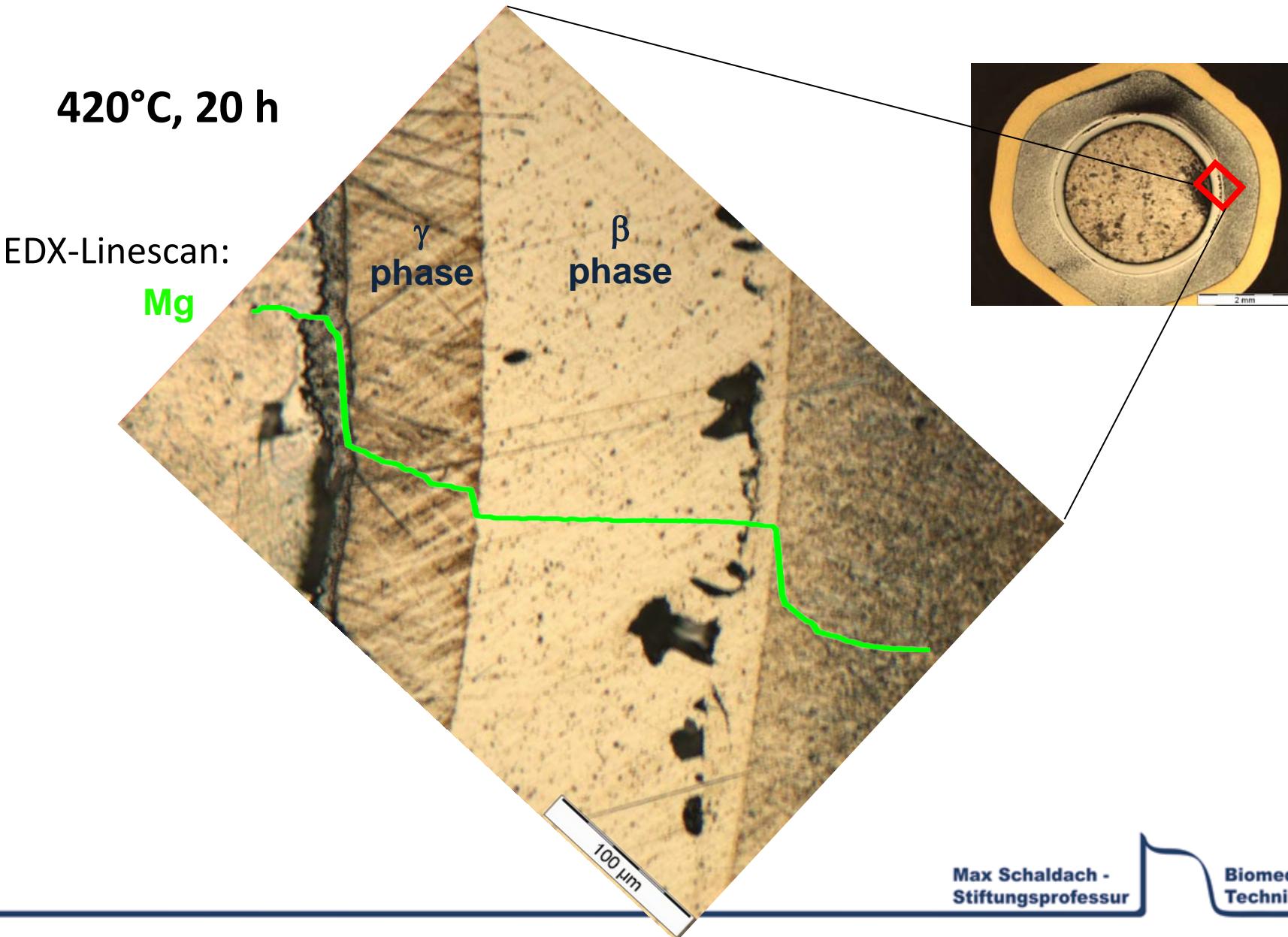


Infinite reservoir experiments

Experimental Setup



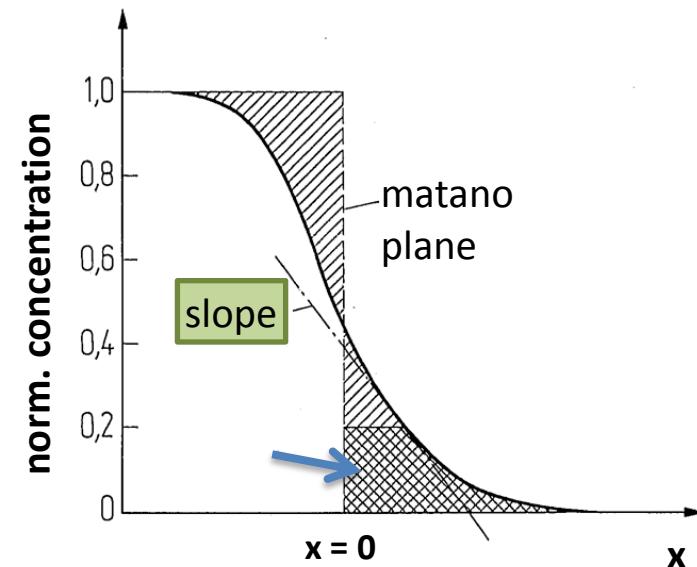
Measurements



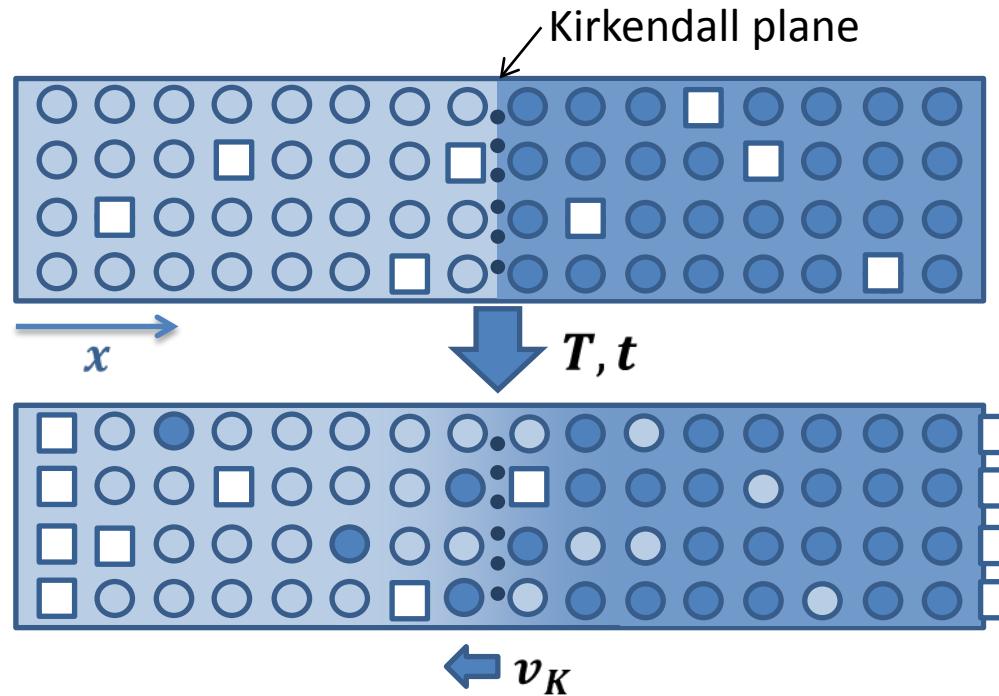
Boltzmann-Matano Method

- Determination of interdiff. coeff. $\tilde{D}(C)$
- EDX-Linescans yield $C(x)$
- Matano plane: $\int_0^1 x \, dc' = 0$

$$\tilde{D}(c) = -\frac{1}{2t} \left(\frac{dx}{dc} \right)_c \int_0^c x \, dc'$$



Darken Equation

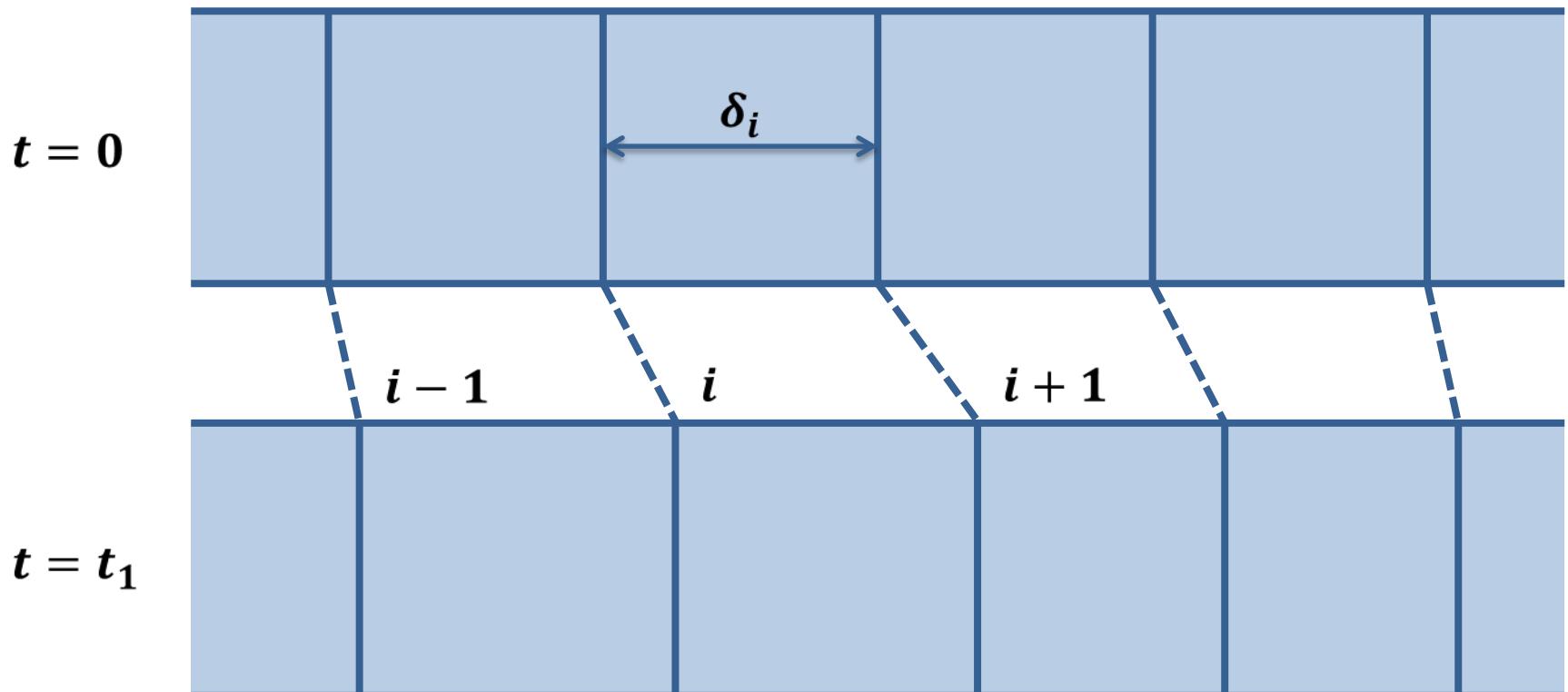


$$J_x = -D \frac{\partial C}{\partial x} \pm v_K C$$

$$v_K = \tilde{V}(D_1 - D_2) \frac{\partial C}{\partial x}$$

$$J_x = -\tilde{D} \frac{\partial C}{\partial x} \quad \text{with} \quad \tilde{D} = X_1 D_2 + X_2 D_1$$

Simulation - Setup



Indices:

i = position

k = component

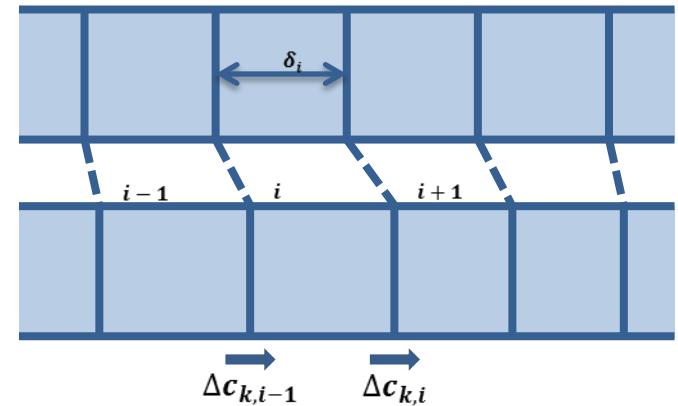
Simulation - Parameters

Parameters:

$D_{k,i}$ = effective diffusion coefficient

$c_{k,i}$ = concentration

$X_{k,i}$ = mole fraction



Indices:

i = position

k = component

Simulation - Algorithm

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2} \xrightarrow[\text{method}]{\text{finite difference}} \Delta c_{k,i} = -D_{k,i} \frac{c_{k,i+1} - c_{k,i}}{(x_{k,i+1} - x_{k,i})^2} \Delta t$$

~~$c_{k,i}(t + \Delta t) = c_{k,i}(t) + \Delta c_{k,i-1} - \Delta c_{k,i}$~~ not valid, as $\Delta c_{k,i}$ also changes δ_i

→ Therefore we use the relative amount of substance $n_{k,i}^*$

Simulation - Parameters

Parameters:

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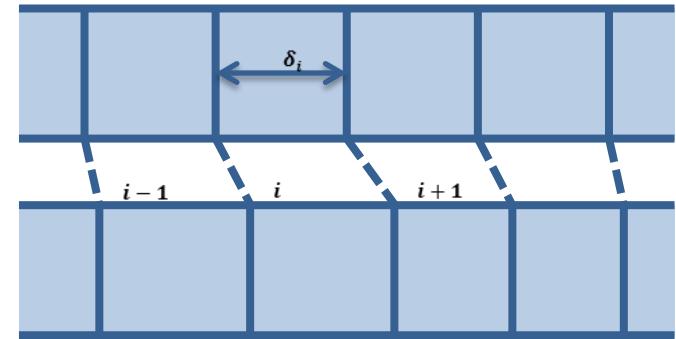
$c_{k,i}$ = concentration

$X_{k,i}$ = mole fraction

$$\tilde{V}_i = \sum_k X_{k,i} \cdot \tilde{V}_k = \text{molar volume}$$

$$n_i = \frac{V_i}{\tilde{V}_i} = \text{amount of substance}$$

$$\left. \begin{aligned} n_i^* &= \frac{\delta_i}{\tilde{V}_i} \\ n_{k,i}^* &= \delta_i \cdot c_{k,i} \end{aligned} \right\} = \text{relative amount of substance}$$



Indices:

i = position

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~~$c_{k,i}(t + \Delta t) = c_{k,i}(t) + \Delta c_{k,i-1} - \Delta c_{k,i}$~~ not valid, as $\Delta c_{k,i}$ also changes δ_i

Therefore we use the relative amount of substance $n_{k,i}^*$

$$n_{k,i}^*(t + \Delta t) = n_{k,i}^*(t) + \Delta c_{k,i-1} \cdot \delta_{i-1}(t + \Delta t) - \Delta c_{k,i} \cdot \delta_i(t + \Delta t)$$

$n_{k,i}^*; \delta_{i-1}; \Delta c_{k,i-1}$ Known from previous steps

$\delta_i(t + \Delta t)$ Dependent on $n_i^*(t + \Delta t)$

Simulation - Algorithm

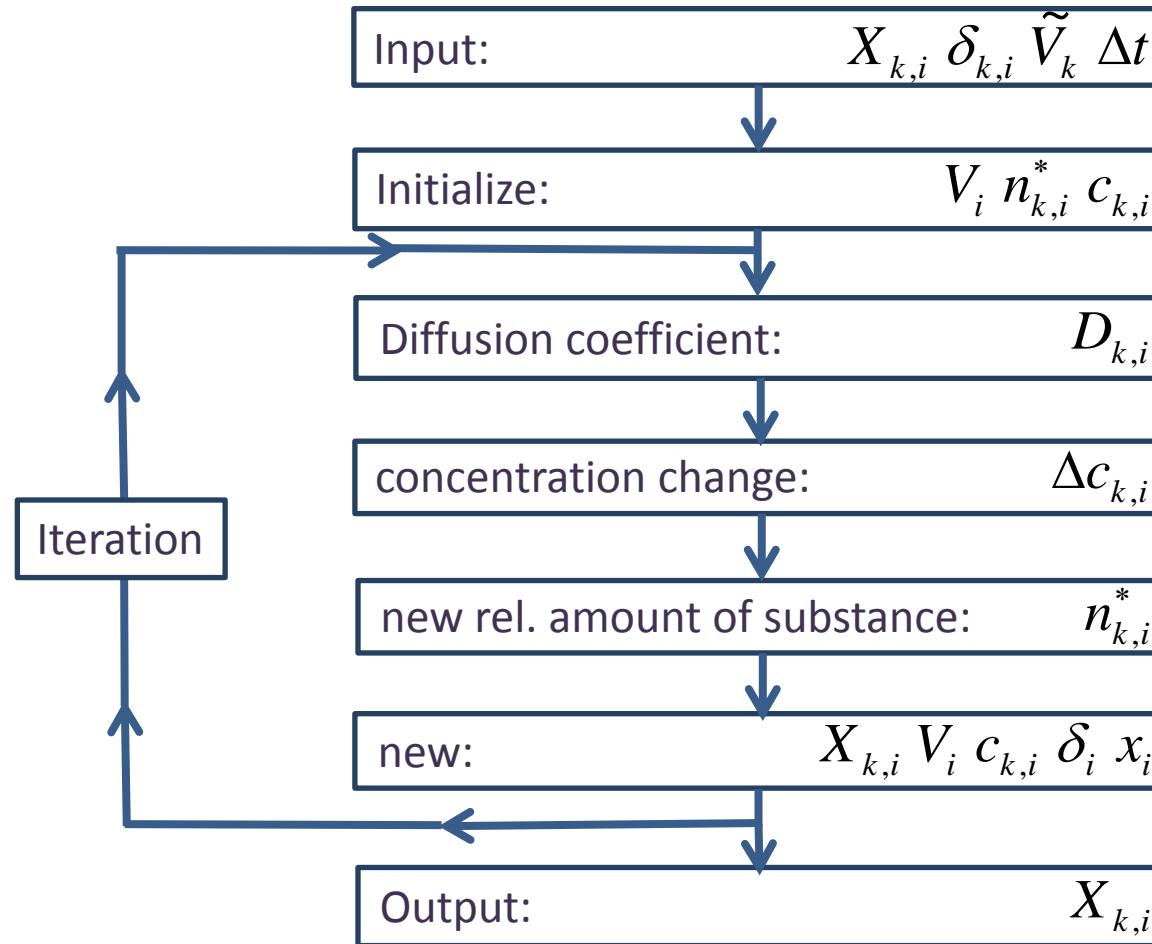
... a few calculations later ...

$$n_{A,i}^* = \frac{n_{A,i}^{re} (1 + \Delta c_{B,i} \tilde{V}_B) - n_{B,i}^{re} \Delta c_{A,i} \tilde{V}_B}{1 + \Delta c_{A,i} \tilde{V}_A + \Delta c_{B,i} \tilde{V}_B}$$

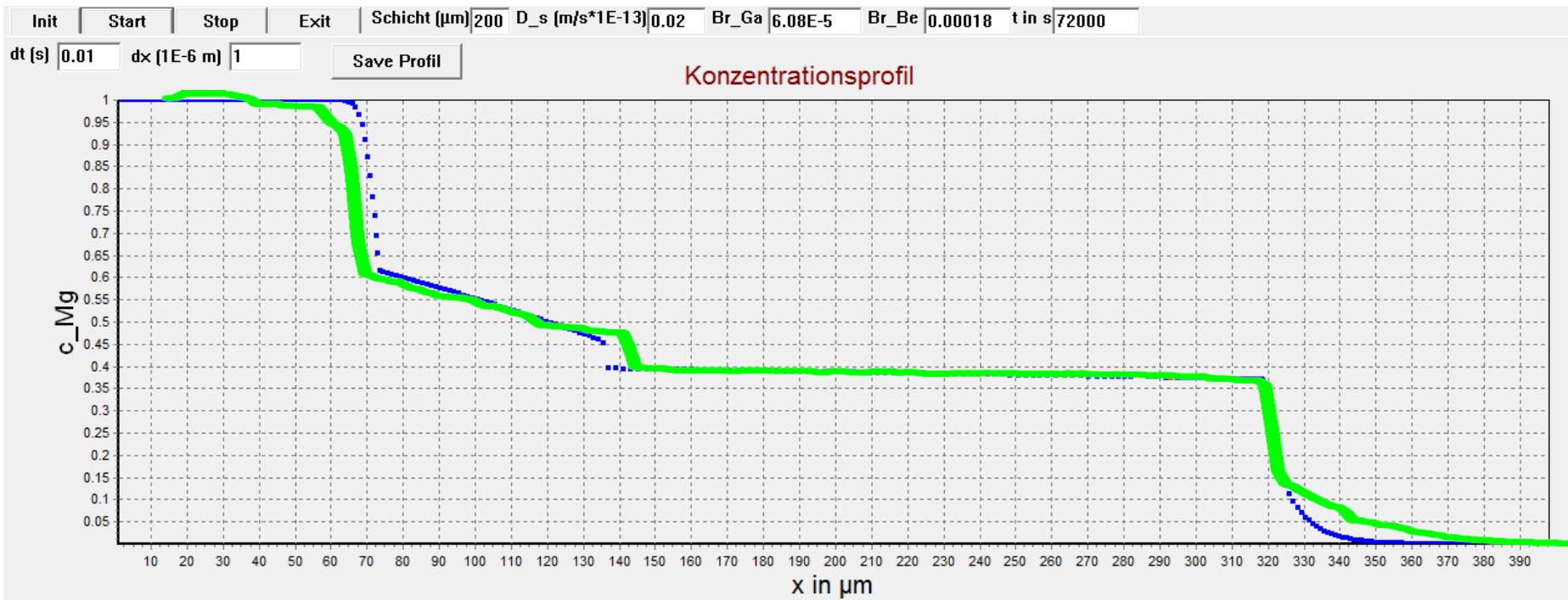
$$n_{B,i}^* = \frac{n_{B,i}^{re} (1 + \Delta c_{A,i} \tilde{V}_A) - n_{A,i}^{re} \Delta c_{B,i} \tilde{V}_A}{1 + \Delta c_{A,i} \tilde{V}_A + \Delta c_{B,i} \tilde{V}_B}$$

$$n_{k,i}^{re} = n_{k,i}^*(t') + \Delta c_{k,i-1} \delta_{i-1}(t' + \Delta t)$$

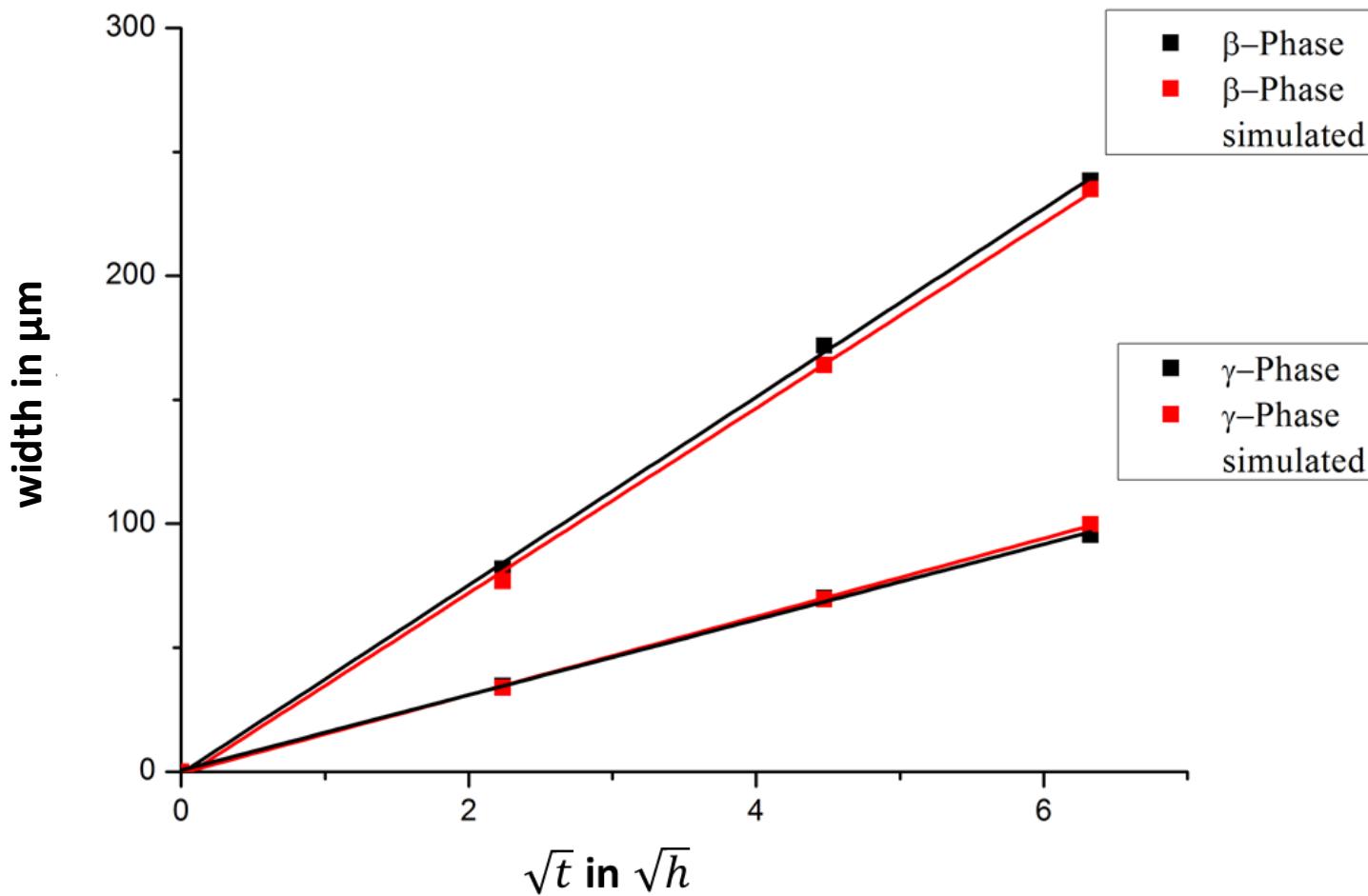
Simulation - Algorithm



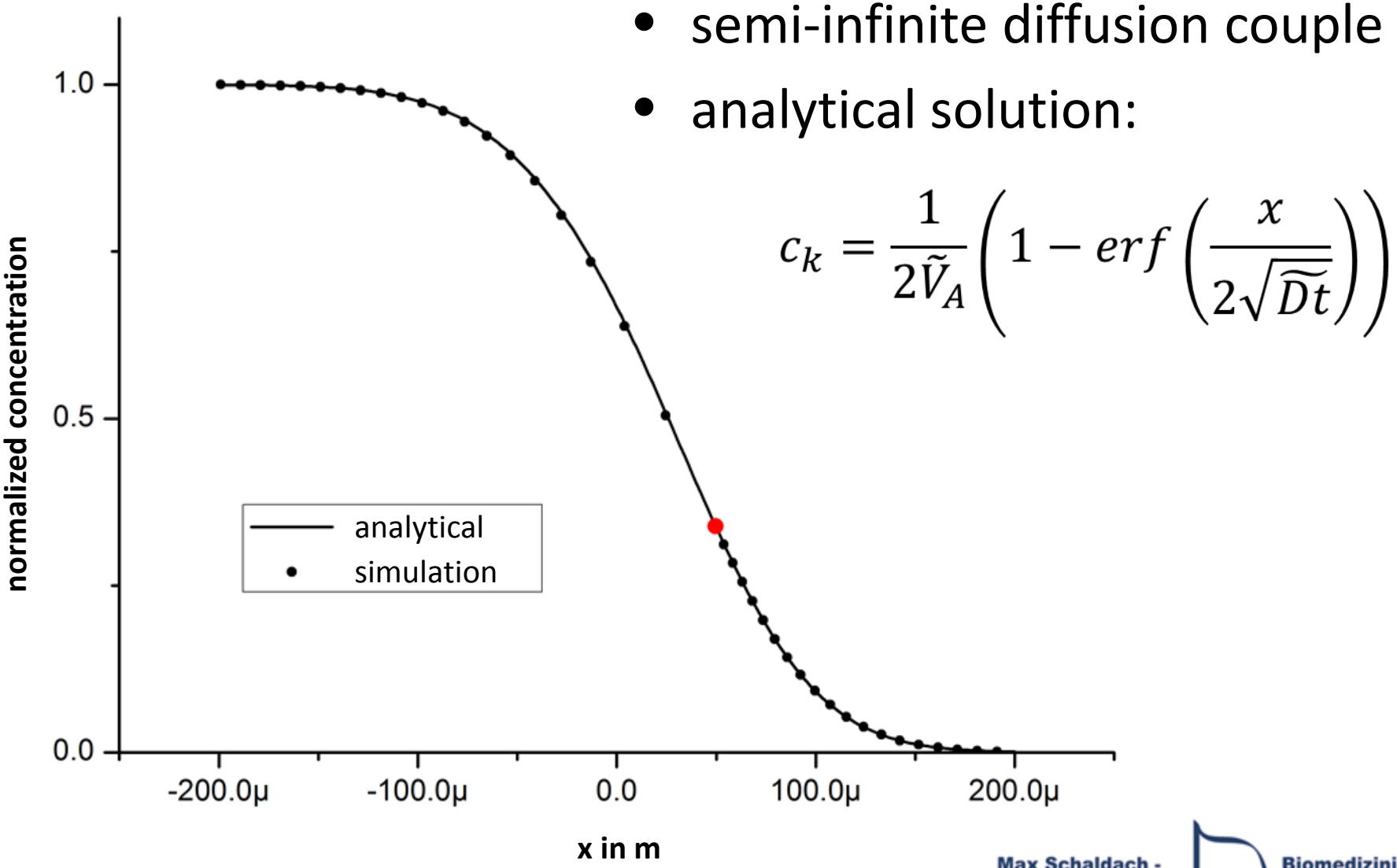
Simulation vs. Measurement



Simulation vs. Measurement



Simulation vs. Analytical Solution



Demonstration, Questions and Discussion

Thank you for your attention

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