

# Corrosion of metals



MB - JASS 09

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## Outline

- corrosion of metals in aqueous solutions
- corrosion processes
  - (material, biomaterial, current density potential diagram)
- Pourbaix-diagram
- different types of corrosion
  - surface corrosion
  - pitting corrosion
- corrosion of metals
  - titanium
  - ion
  - 316L
  - magnesium
- Stents
  - ion
  - magnesium



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# Corrosion

**What is corrosion?**

**Definition (DIN 50900):**

- Reaction of a material with the environment
- Measurable change (properties, behavior)
- Probably damage of a function or system

**Appearance:**

*Basically electrochemical*

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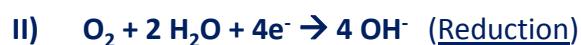
# Corrosion

Generic chemical formula for anodic metal loss:



The produced **electrons** are **consumed** at the cathodic side:

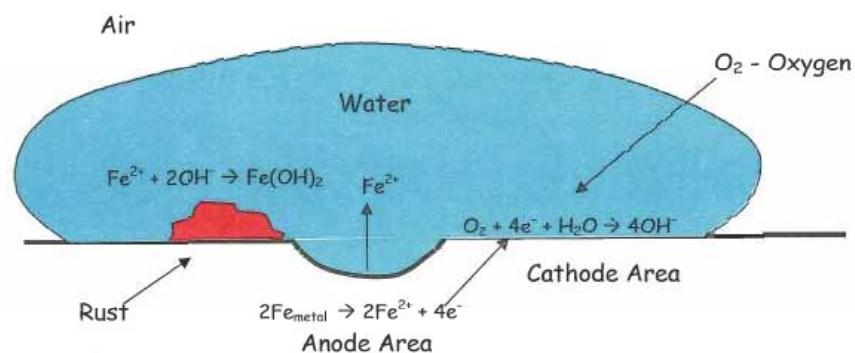
→ 2 possibilities in aqueous solution:



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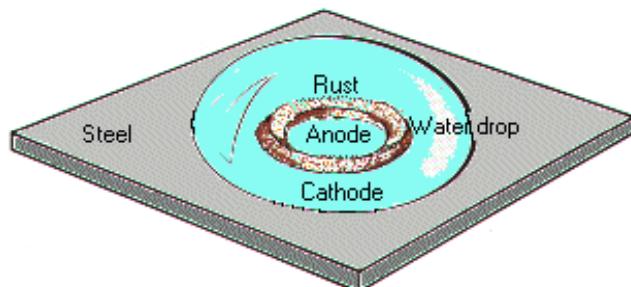
## Corrosion

### Corrosion of iron (Fe) :



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## Corrosion



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## Corrosion

Only noble metals are stable in aqueous environment

→ Oxidation-potential > Reduction-potential  
(noble metal) (environmental species)

Other reason for stability:

→**PASSIVITY:** stable non-dissolvable **oxide-layer** on the surface  
→ primarily **titanium!**

## Corrosion

Electrode	Electrode reaction	$E^\circ/V$
Au Gold	$Au^{3+} + 3e^- \rightleftharpoons Au$	+1.43
Ag Silver	$Ag^+ + e^- \rightleftharpoons Ag$	+0.80
Cu Copper	$Cu^{2+} + 2e^- \rightleftharpoons Cu$	+0.34
H Hydrogen	$H^+ + e^- \rightleftharpoons H$	0
Pb Lead	$Pb^{2+} + 2e^- \rightleftharpoons Pb$	-0.13
Sn Tin	$Sn^{2+} + 2e^- \rightleftharpoons Sn$	-0.14
Ni Nickel	$Ni^{2+} + 2e^- \rightleftharpoons Ni$	-0.25
Cd Cadmium	$Cd^{2+} + 2e^- \rightleftharpoons Cd$	-0.40
Fe Iron	$Fe^{2+} + 2e^- \rightleftharpoons Fe$	-0.44
Zn Zinc	$Zn^{2+} + 2e^- \rightleftharpoons Zn$	-0.76
Ti Titanium	$Ti^{2+} + 2e^- \rightleftharpoons Ti$	-1.63
Al Aluminum	$Al^{3+} + 3e^- \rightleftharpoons Al$	-1.66
Mg Magnesium	$Mg^{2+} + 2e^- \rightleftharpoons Mg$	-2.37
Na Sodium	$Na^+ + e^- \rightleftharpoons Na$	-2.71
K Potassium	$K^+ + e^- \rightleftharpoons K$	-2.93
Li Lithium	$Li^+ + e^- \rightleftharpoons Li$	-3.05

↑: noble metals, cathode

↓: base metals, anode

$$\Delta U = E_{\text{anode}} - E_{\text{cathode}}$$

< 0 → reaction possible!

→ Actually **titanium** is less noble,  
**but:** high O<sub>2</sub>-affinity: formation of a  
protective oxide-layer

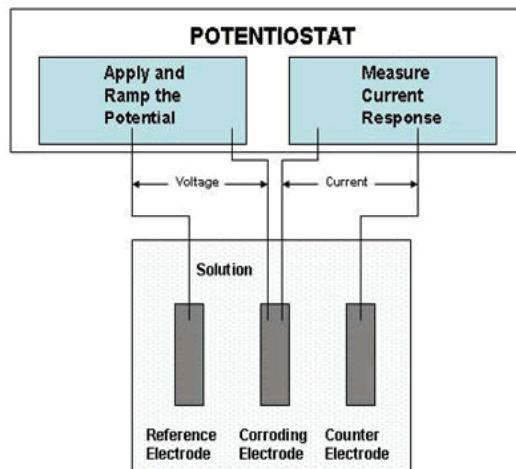
## Corrosion

### Correlation: Current Flow and Weight Loss

- Metal loss is proportional to the produced electrons
- Metal loss is proportional to the current flow
- Corrosion-rates can be determined by applying current ( $j$ ) against potential ( $E$ )

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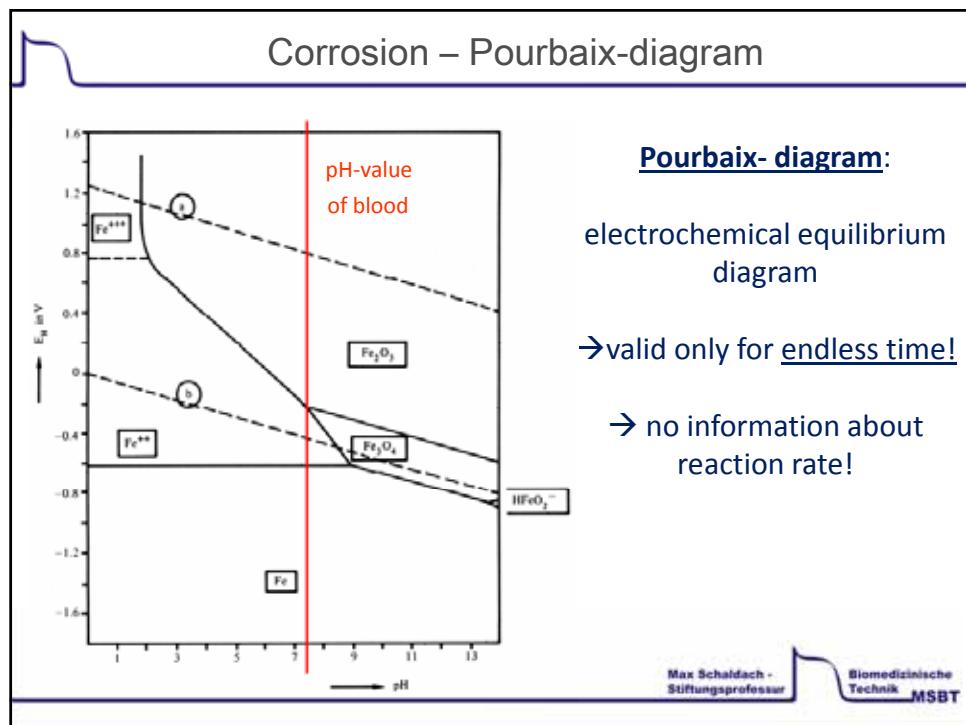
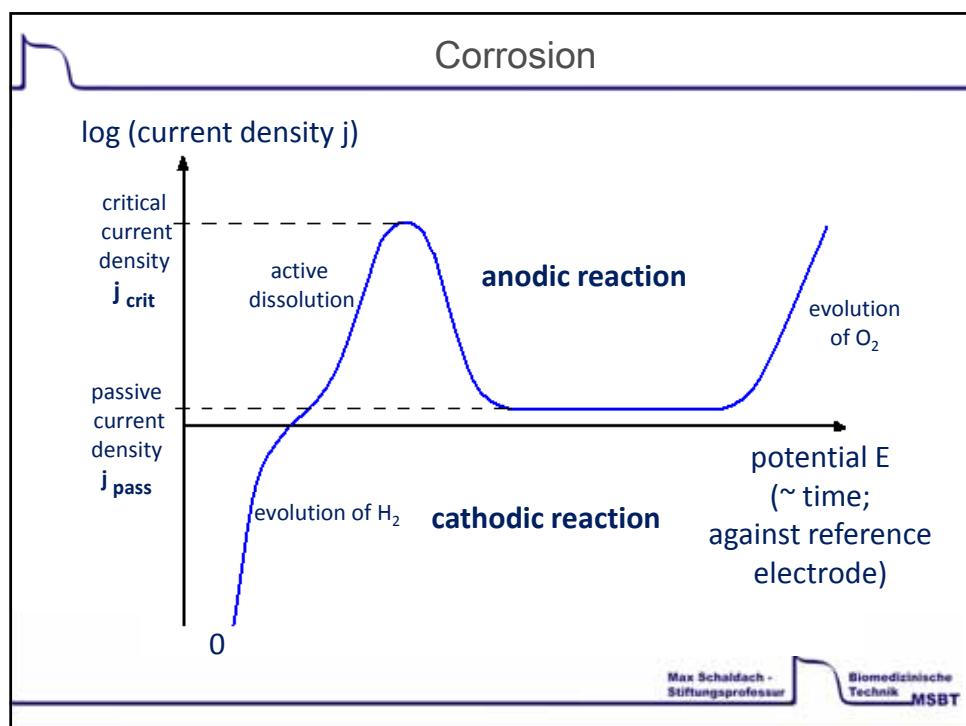
## Corrosion



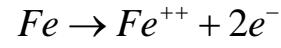
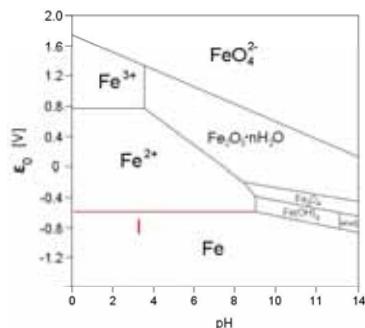
### Measurement of $j/E$ -curve:

- Voltage-setting between **corroding electrode** and **reference electrode**
- Current between **corroding electrode** and **counter electrode**
- The **reference electrode** keeps its potential (high-ohmic input)

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## Corrosion – Pourbaix-diagramm

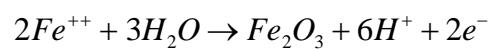
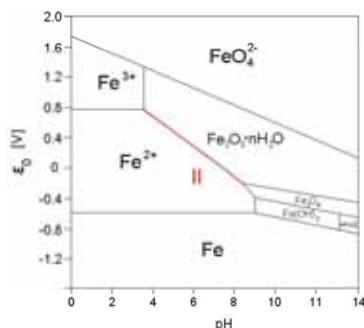


$$E_{\text{Fe}/\text{Fe}^{++}} = E_{\text{Fe}/\text{Fe}^{++}}^0 + \frac{0,059}{2} \cdot \lg c_{\text{Fe}^{++}}$$

$$E_{\text{Fe}/\text{Fe}^{++}} = -0,62 \text{ Volt}$$

→ No pH-value dependance: **horizontal line I**

## Corrosion – Pourbaix-diagramm

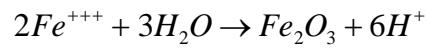
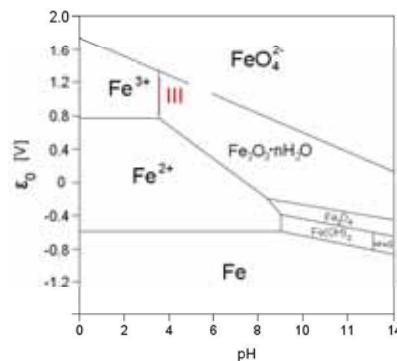


$$E_{\text{Fe}/\text{Fe}_2\text{O}_3} = E_{\text{Fe}/\text{Fe}_2\text{O}_3}^0 + \frac{0,059}{2} \cdot \lg \frac{c_{\text{H}^+}^6}{c_{\text{Fe}^{++}}^2}$$

$$E_{\text{Fe}/\text{Fe}_2\text{O}_3} = 1,09 - 0,18 \text{ pH}$$

→ pH-value-dependance: **line II**

## Corrosion – Pourbaix-diagramm



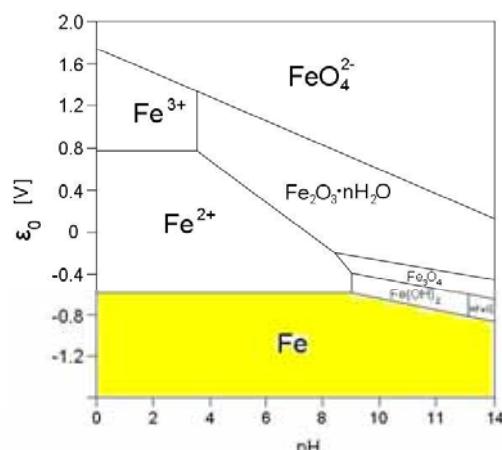
$$\frac{c_{\text{H}^+}^6}{c_{\text{Fe}^{+++}}^2} = K = 10^{1,45}$$

$$p\text{H} = 1,76$$

→ pure chemical reaction: vertical line III

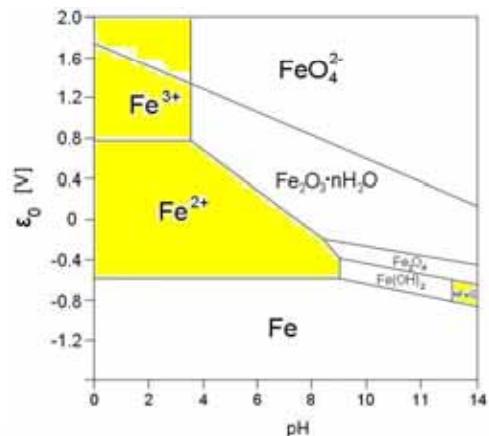
## Corrosion – Pourbaix-diagramm

Yellow: inert area



## Corrosion – Pourbaix-diagram

Yellow: corrosion area

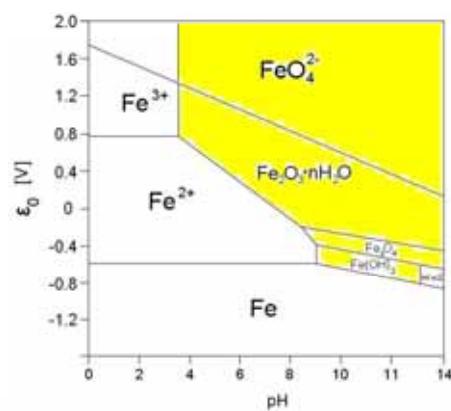


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## Corrosion – Pourbaix-diagram

Yellow: areas with stable oxides



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## Corrosion

### Corrosion of implants in human body:

→ Blood = complex electrolyte

\* pH = 7,4 ( $\pm 0,05$ ) → generated with a buffer-system

\* blood consists of cells and plasma (proteins and electrolytes like  $Cl^-$  or  $PO_4^{3-}$  dissolved in water)

→ more aggressive than seawater!

→ Corrosion increased at areas with **mechanical stress**

→ Can provoke an **inflammation**

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## Corrosion

### How do metallic ions damage the tissue?

- I) Ph- value and the oxygen partial pressure can diversify and this can change the chemical environment  
(metal-ions form heavily solvable compounds)
- II) Metallic ions can change the cell-metabolism

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## Different types of corrosion

### corrosion

- surface corrosion
- atmospheric corrosion
- galvanic (contact) corrosion
- ...

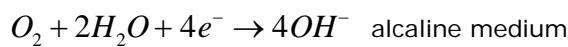
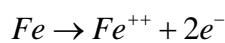
### types of local corrosion

- pitting corrosion
- crevice corrosion
- stress-cracking corrosion
- intercrystalline corrosion
- ...

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## Surface corrosion

### mechanism:



### preconditions:

- conductive surrounding (even a very thin water film is enough)
- homogeneity of surrounding & material

! anodic and cathodic reactions are parallel !

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## Galvanic corrosion

→ dissimilar conducting materials are connected electrically and exposed to an electrolyte

preconditions:

- electrochemically dissimilar metals
- metals are in electrical contact
- metals are exposed to an electrolyte



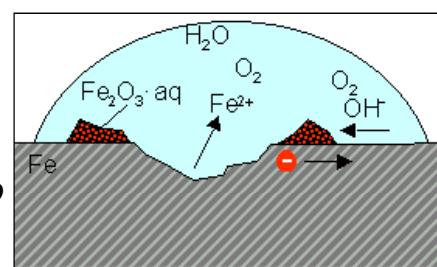
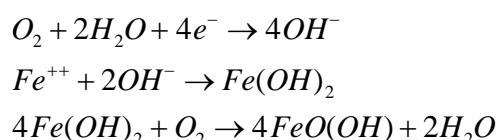
metals in electrolyte → different corrosion potentials of different metals  
→ potential difference = driving force for galvanic current flow

less noble material = anode → acceleration of corrosion  
more noble material = cathode → reduction of corrosion

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## Pitting corrosion

- Kathodic reaction at the periphery of the drop
- Passivation of border area by increasing pH
- Low pH & low O<sub>2</sub>-concentration in the middle → dissolving of ion
- around anodic area: formation of rust

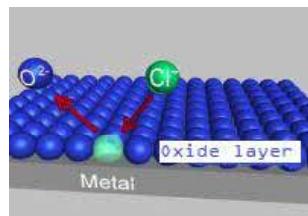


↑Corrosion with ↓O<sub>2</sub> concentration

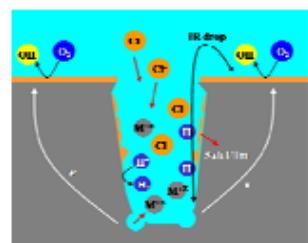
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## Pitting corrosion

Initiation:  
Oxide layer  
breakup



Processes in  
the pit



pitting corrosion on  
surface of cast iron bathtub



[23] [24]

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## Influences on corrosion

- pH → Porbaix-diagram
- microstructure → galvanic elements
- temperature → ↑ diffusion constant  
→ ↓ O<sub>2</sub>-conc. in open systems
- O<sub>2</sub>-concentration → drop-model
- velocity of flow
- salt-concentration

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## Corrosion of metals

Examples:  
titanium  
iron  
316L  
magnesium

## Titanium

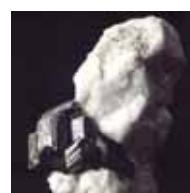
## Implants

properties	bone	magnesium	Ti-alloy	Co-Cr-alloy	316L
<b>density (g/cm<sup>3</sup>)</b>	1,8-2,1	1,74-2,0	4,4-4,5	8,3-9,2	7,9-8,1
<b>Young's modulus (GPa)</b>	3-20	41-45	110-117	230	190
<b>fracture toughness (MPam<sup>1/2</sup>)</b>	3-6	15-40	55-115		0,7

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## Titanium



rutil

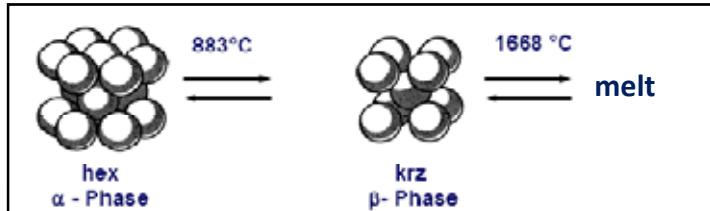


anatas



brookit

### structures



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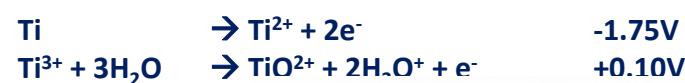
Titanium

Corrosion Resistance ?

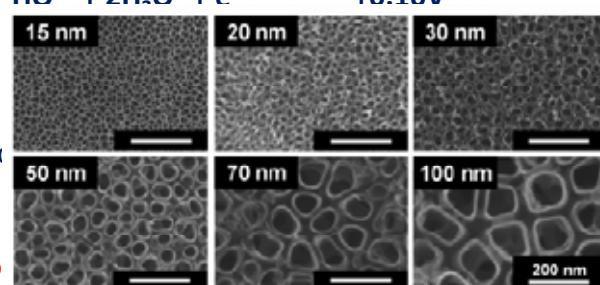
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Titanium

Ti: creation of a titanium oxide layer  
→ good corrosion resistance



$\text{TiO}_2$   
→ n-type semiconductor  
→ amorphous  
→ anodisation: crystal  
= under specific electro



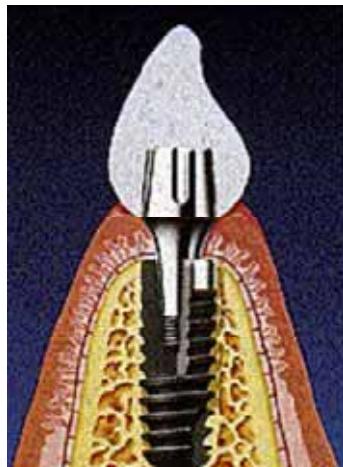
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## Passivation of Titanium

→ titanium oxide layer  $\text{TiO}_2$

→ highly stable surface oxide layer provides excellent corrosion resistance

## Titanium - applications

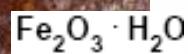
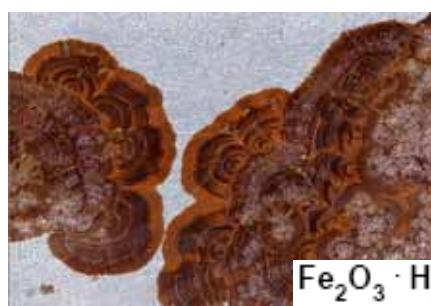


## Iron

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## Iron (Fe)

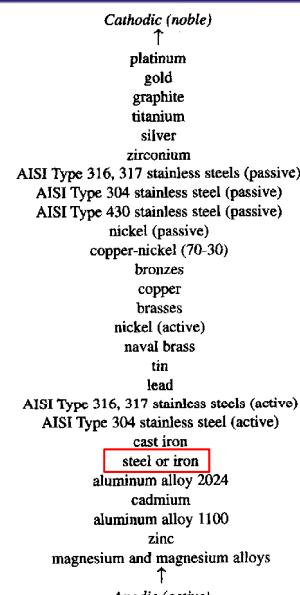
- 4,7 wt.-% of earth crust
- **Resistant** in dry air, in dry Cl,  
concentrated sulfuric acid and  
in alkaline medium (except  
 $\text{NaOH}$  with  $\text{pH} > 9$ )



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## Iron (Fe)

The more active metal in the galvanic couple becomes the anode and gets oxidized. The noble metal is the cathode.



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316L

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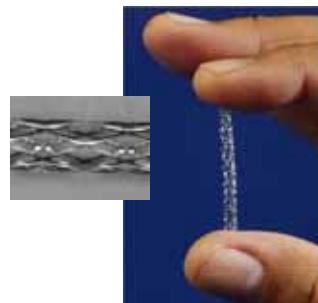
## 316 L

Surgical stainless steel is a specific type of stainless steel, used in medical applications

### Elemental composition

Wt.-%

	316L
C	<0.03
Cr	17-19
Ni	12-14
Mo	2-4



- Low content of C
- High addition of Cr and Ni

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## 316 L

Corrosion Resistance ?

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## 316 L

Formation of a compact oxide layer ( $\text{Cr}_2\text{O}_3$ )

→ protection against corrosion

but...

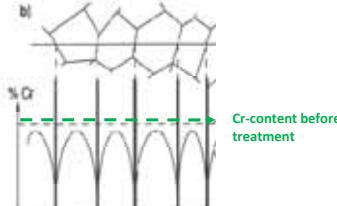
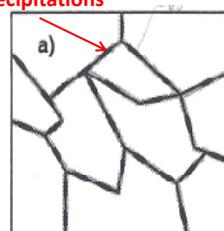
Thermal treatments (welding, annealing) lead to  $\text{Cr}_{23}\text{C}_6$ -precipitations in the grain boundaries



→ Inside the grain decreased Cr-concentration

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Cr<sub>23</sub>C<sub>6</sub>-precipitations

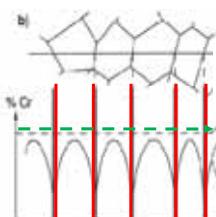


- Cr-precipitations at the grain boundaries
- Less Cr near the grain boundaries

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## 316 L

Cr<sub>23</sub>C<sub>6</sub>-precipitations



After thermal treatment:  
high Cr-content at grain  
boundaries

Cr-content before  
treatment

After treatment

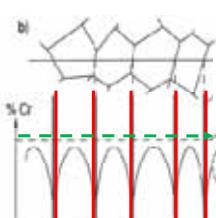
- Less Cr near the grain boundaries
  - Critical passivation current density increases
  - **Possibility to lose passivation**

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## 316 L

Cr<sub>23</sub>C<sub>6</sub>-precipitations



After thermal treatment:  
high Cr-content at grain  
boundaries

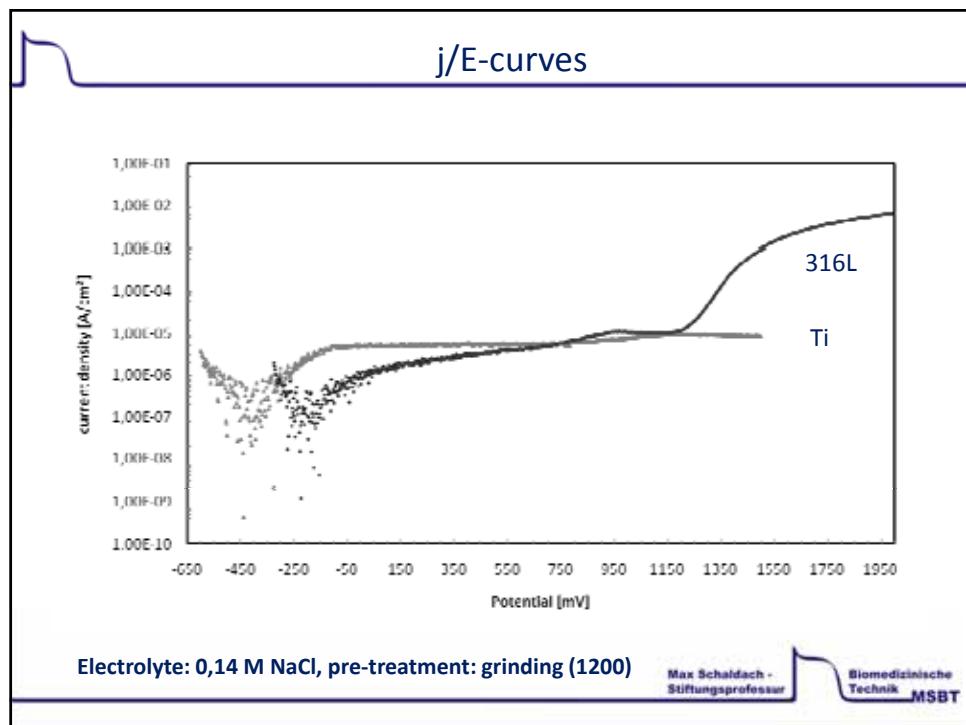
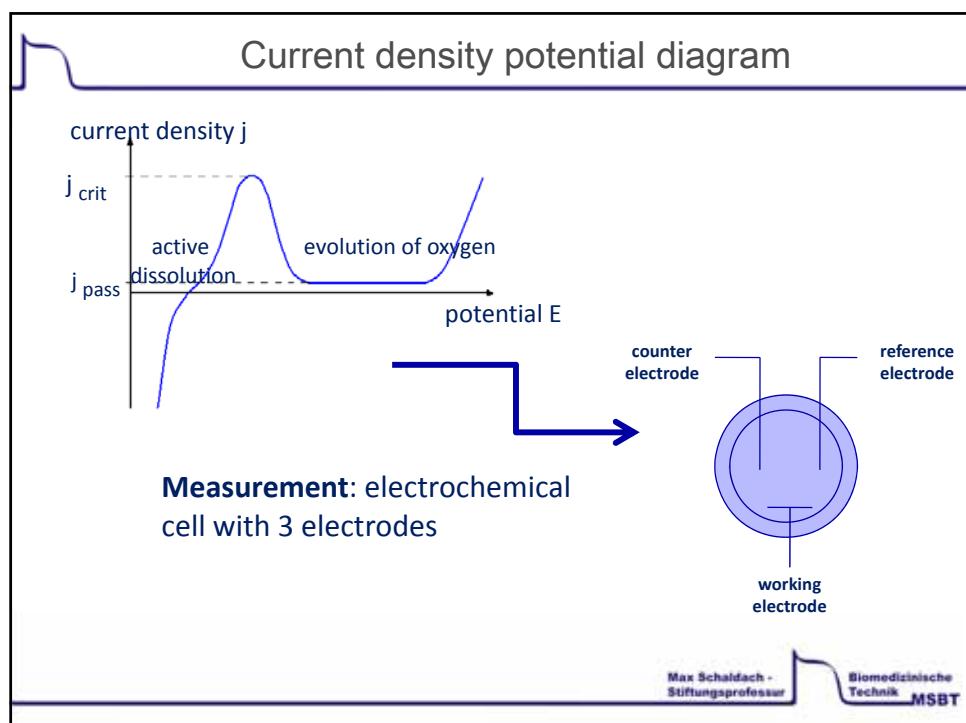
Cr-content before  
treatment

After treatment

- Different concentrations near the grain boundaries and in the grain boundaries
  - **Danger of contact corrosion**

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## 316L



→ mainly protection

but

→ pitting caused by  
chloride-ions

Microscopic picture of 316L after  
electrochemical treatment

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## Titanium



→ Leveling of grinding  
grooves because of  
grown oxide layer

Microscopic image of Ti after  
electrochemical treatment

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## Magnesium

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## Implants

properties	bone	magnesium	Ti-alloy	Co-Cr-alloy	316L
density (g/cm <sup>3</sup> )	1,8-2,1	1,74-2,0	4,4-4,5	8,3-9,2	7,9-8,1
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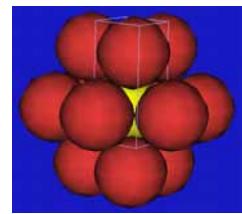
## Magnesium



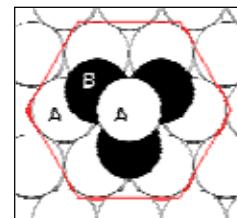
magnesium  
1.74 g/cm<sup>3</sup>

12	24,305
1107	651
<b>Mg</b>	
Magnesium	

atomic number  
atomic mass  
symbol  
name  
boiling temperature  
melting point



Hexagonal-closed-packed



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## Magnesium

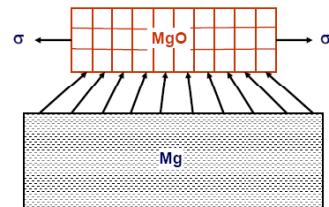
Corrosion Resistance ?

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## Magnesium

**Mg:** highly negative electrochemical potential of -2.38 V

→ low corrosion resistance



**MgO:** no formation of protection layer

WHY? → difference in molar volume of Mg & MgO

→ flaking off caused by tensile & compression stresses

Mg → corrosion even in water

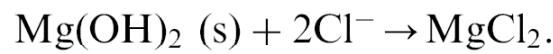
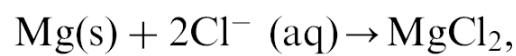
Mg in acids → highest corrosion

increase of corrosion rate by impurities in Mg – especially Fe, Ni, Cu

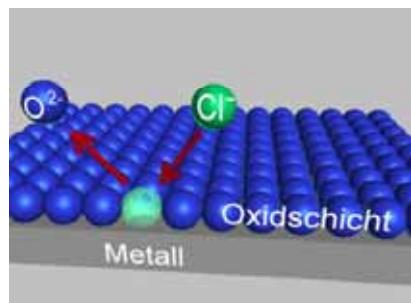
→ galvanic corrosion

## Magnesium

### corrosion reactions of magnesium



## Magnesium-corrosion

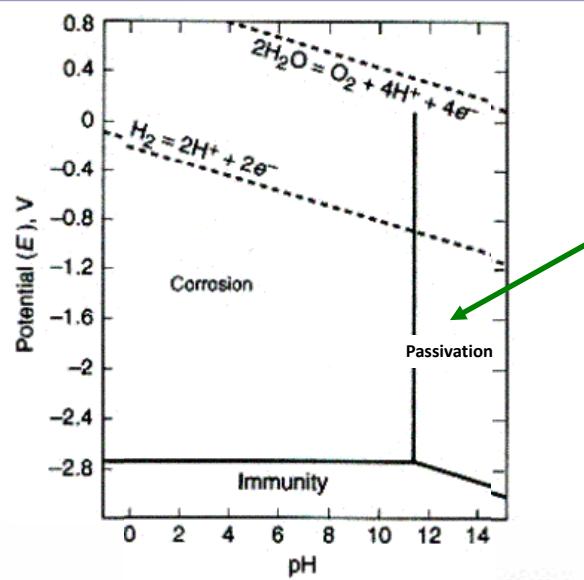


- local corrosion of passive layer by  $\text{Cl}^-$
  - rapid increase of corrosion rate
- pitting corrosion

	$\text{Na}^+$	$\text{K}^+$	$\text{Mg}^{++}$	$\text{Cl}^-$
Blut [mmol/l]	142,0	3,6-5,5	1,0	95,0-107,0

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## Pourbaix-diagram of Mg



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## Magnesium

Mg-corrosion in the body?

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## Magnesium – corrosion in the body?

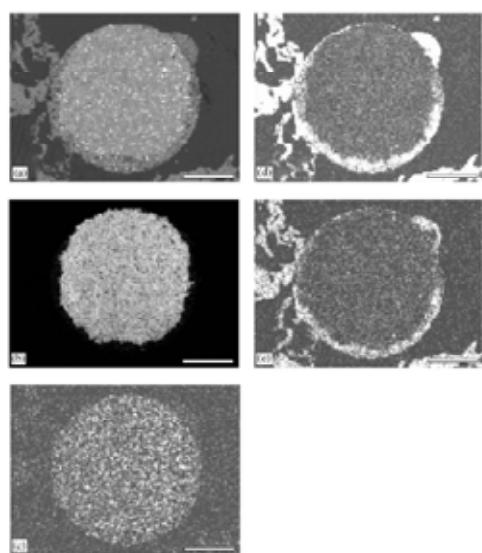
### Simulated body fluid

	1 Liter SBF/ ml
KCl	5.63
NaCl	59
NaHCO <sub>3</sub>	18
MgSO <sub>4</sub> *7H <sub>2</sub> O	5
CaH <sub>2</sub> bzw. CaCl <sub>2</sub>	25
TRIS	50
NaN <sub>3</sub>	10
K <sub>2</sub> HPO <sub>4</sub>	5.25

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## Magnesium – corrosion in the body



Biomaterials 26 (2005) 3557–3563

### EDX analysis:

- degraded implant: replaced by a conversion layer containing mainly Ca & P
- rare earth elements were distributed homogeneously in the corrosion layer & in the remaining implant material but not in the surrounding bone

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## Magnesium – corrosion in the body



Subcutaneous gas bubbles observed on postoperative radiographs for 4 weeks during magnesium implant degradation

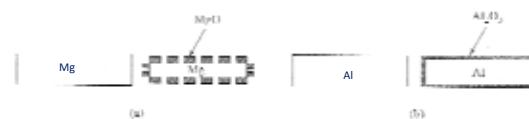
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## Oxide layers – specific volume

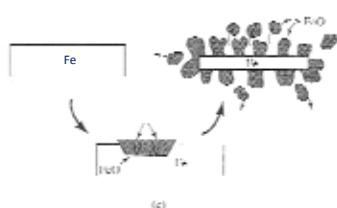
P-B-Ratio < 1



P-B-Ratio = 1-2



P-B-Ratio > 2



$$\text{Pilling - Bedworth - Ratio} = \frac{\text{oxide volume per metal atom}}{\text{metal volume per metal atom}} = \frac{(M_{\text{oxide}})(\rho_{\text{metal}})}{n(M_{\text{metal}})(\rho_{\text{oxide}})}$$

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## Stents



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## Bioabsorbable stents

Possible Materials??

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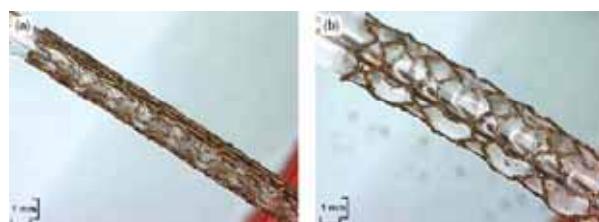
## Bioabsorbable iron stents

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## Bioabsorbable Iron Stent

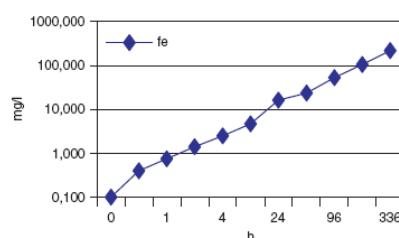
- Iron is an essential element (daily need: 0,5-5 mg)
- stent weighs about 40 mg (coronary) or 250 mg (peripheral)
- low toxicity, because of the low rate of corrosion
- systemic toxicity is not to be anticipated even after implantation of multiple stents



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## Bioabsorbable Iron Stent

Studies with **pure iron** (less than 1 % contamination) foils (diameter 26 mm, thickness 0,91 mm) in **electrolyte**:

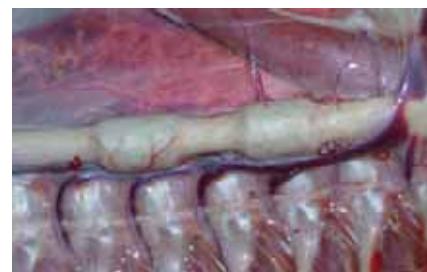


→ Loss of 15 % mass after 1 week's incubation in human serum

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## Bioabsorbable Iron Stent

In vivo studies



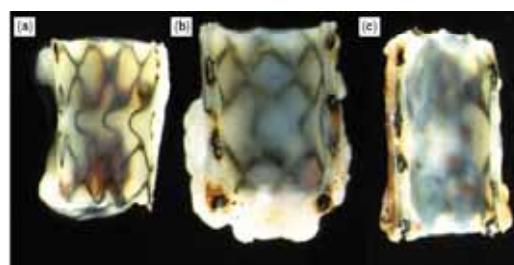
12 months after implantation: corrodible **iron stent** (left) and **316L stent** (right) in the descending aorto of a minipig

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## Bioabsorbable Iron Stent

**Macroscopic aspect of corrosion process** 3 (a), 6 (b) and 12 (c) months after implantation



- (a) Struts of the stents are clearly visible, corrosion plaques limited to the intersections
- (b) Progressive loss of structure, accumulation of corrosion products
- (c) Loss of integrity

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## Biodegradable magnesium stents

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### Reasons for favoring Mg as stent material

- Hypothrombotic properties
- Predictable tissue tolerance
- Mechanical properties: Outstanding stability-to-mass ratio
- Therapeutically used
- Vasodilating properties:  
  
As a physiologic calcium antagonist,  
magnesium inhibits the muscle contraction  
and thus the tone of vessels.

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## Bioabsorbable magnesium-stent

1 stent (1.1 mm × 10 mm):  
≈ 4 mg magnesium



0.7 l drinking water:  
≈ 110 mg magnesium



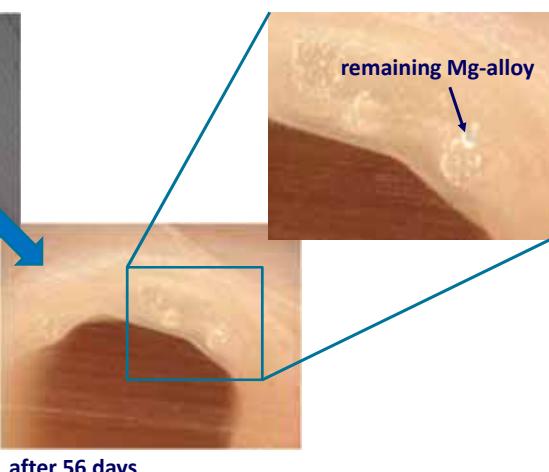
- Mg → essential mineral:
  - 20 g in human bodies
  - 350 mg recommended ingestion per day
- Mg → relaxation of muscles
- Mg → very low allergen reactions

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## Degradation of Mg-stents

Mg-alloy  
conversionlayer  
after 14 days



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Thank you for your attention!

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